

67 Chevelle SS396 Project

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Mission Statement

To build a unique show winning 67 Chevelle SS396 that is a pleasure to look at and drive on the street and is a very fast and capable performer at the strip.

- Will meet all of the NHRA safety requirements for a 7.50 to 10.99 index car
- Will run 9.90s with on the motor with 10" slicks, 10's with DOT tires
- Will run 8.90s on the bottle with 10" slicks
- Will have 4 wheel disk brakes, modern steering and suspension
- The exterior and interior will be as "stock" looking as possible. This will include the use of the stock hood and the possible restriction of using a dual plane intake manifold – even for racing
- Will pass emissions air care test for model year
- Will be highly reliable, strong and well built

Introduction

This document is in its very first draft version. When it is finished it will detail the complete story of the creation of the final car – the people and their businesses and their relationships to each other, the technology, the ups and downs and the results – complete with color pictures.

For now, this document remains a skeleton of the final version and is only documenting the engine dyno testing results obtained so far and the necessary changes to the engine design before making the next set of dyno pulls.

Enjoy!

The People and Companies behind this Project

I would like to thank the following companies and individuals who have been instrumental in this project's successful completion (TBD!):

Kelly Hildebrandt, Lake Cowichan

... for selling me a clean unmolested car in the first place (so that I can molest it first)

Summit Racing, Ohio - Redd

... for the incredible sales support involving almost every component that is new (most of the car) and technical support which involved countless calls to suppliers and dozens of faxes and shipments

Import Automotive, Vancouver – Loyd, Fritz and the gang

... for performing the initial teardown, and the installation of the front suspension, rear suspension (partially going into storage), GM 12 bolt prep (going into storage), brake system, and steering system. Loyd also introduced me to the gang at Pacific Parts, Spirit Engineering, and Kyles Classics.

Pacific Parts, Vancouver – Peter, Terry and Rick

... for building the first Mark VI BB Chevy on the planet and resolving many tricky problems successfully. And for introducing me to Ron Par.

Kyles Classics, Surrey – Kyle and Doug

... for getting the complete chassis and interior details right, final assembly done (TBD), and for getting me to the "correct" SS396 concept. And for introducing me to Gary's Autobody.

<u>Gary's Autobody</u>, Richmond – Gary and the gang

... for straightening out an already show winning chassis and making it straighter than straight and for painting it so that a few heads will turn.

Spirit Engineering, Surrey – Stan and Gordon

... for the underbody stiffening, for the very trick 4130 rollcage, the aluminum fuel cell and fuel pump mounts, battery box and trunk sheetmetal, the custom Strange rearend, and front and rear suspension mods and coilovers.

Ron Par Engines, Langley – Ron and Ken

... for the dyno pulls, advice, and some wicked porting of the heads and intake (TBD)

And finally a big thanks to the following suppliers (in addition to the dozens of suppliers represented directly by Summit Racing):

Apple Chevrolet – 502 Mark VI BB engine, hamburger oil pan, water pump

AVO – front racing shocks, rear coilovers

Extrude Hone – intake manifold porting

Global West Suspension – front and rear street suspension, brake system

Jet Hot Coatings – header coatings

JE pistons – custom pistons

K&R – restoration parts for chassis and interior

BG Fuel Systems – filters, pumps, regulators, lines and advice

Be Cool – aluminum radiator

March Performance – engine serpentine pulley system and accessory brackets

Stahl Headers - headers

Turbo Action – shifter, TH-400, converter

The Carb Shop – the carb

Torque Technologies – 3" exhaust system

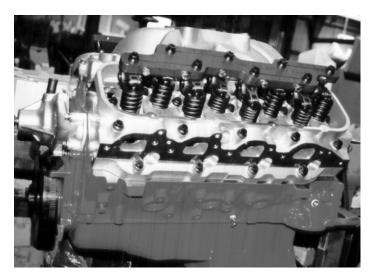
Wheel Vintiques – street wheels

Victory Lane – racing seats and safety equipment

Year 1 – restoration parts for chassis and interior

Engine Development

The engine chosen for this car is the Mark VI 502 BB Chevy. This new for 1997 block shares many of the components with the old Mark IV and newer Mark V but has a number of quality and strength improvements that have been brought about by modern manufacturing techniques. This new block has much tighter tolerances (like a single size piston), added strength (Siamesed walls, taller lifter bosses), 4 bolt bottom end, forged crank, single piece rear main seal, and other reliability changes for marine and high performance use. And to the uneducated eye, it looks just like a 396 under the hood when painted 1960's Chevy orange. Topped off with Aluminum Performer RPM oval-port heads from Edelbrock and the matching Performer RPM dual plane intake manifold, this combo looks a lot like the rare 1967 L78/L89 factory offering.



The characteristics of a good street/strip motor revolve around providing strong low end torque with good upper RPM breathing. Careful engine design should provide a wide, flat torque curve with lots of top end power for the strip. Given the stock under hood clearance limitations, a high rise dual plane manifold without use of a spacer may be the upper limit. Running a single plane intake will require an after market fiberglass hood with a cowl induction or similar setup – not out of the question but far less "stock".

The best route is to maximize engine displacement with a streetable compression ratio (generally thought to be 10.5:1 for 94 octane unleaded gas when using aluminum heads) and also balance the size and flow characteristics of the intake and exhaust system to moderately sized cylinder head port volumes and valve diameters. A solid roller cam with moderate duration and lift should also provide good upper end breathing without killing low end torque and idle vacuum and emissions. Getting the most out of this setup requires careful porting and shaping of the intake and exhaust runners – keeping the velocity up while minimizing restrictions to high RPM air flow.

Running a 9.9 second time slip requires a minimum of 640 hp for a 3400 lbs car. Running an 8.9 requires 920 hp. Both are within reach of the Mark VI 502 when subject to the above constraints with the added help of a 300 hp NOS fogger system for the 8.9 passes. The target hp for this engine combo is 675 hp and 620 ft-lbs of torque on the motor.

First Set of Dyno Tests, May 15-16, 1997

<u>Summary</u>

The engine proved to be remarkably insensitive to changes in the A/F ratio, ignition timing, and even changes to the exhaust system and intake manifolds. In no case did any of the changes produce more than a 2% change in maximum power which is well within the range of repeatability for these types of tests (less than 0.1s and 1mph in the ¹/₄ mile). In fact, the same engine combo tested 1.5% less power on the second day of testing as a back to back reference check. The engine was basically a 600 ft-lbs torque monster on the low end, with approx. 590 hp at 5800 rpm. The dual plane manifold improved torque below 3800 rpm and rolled off slightly faster above 6000 rpm – that was all.

Rather than focus on the small degree of error caused by variations in intake air temperature, pressure and humidity or ignition quality, it is more important to note that these tests indicate that <u>the cylinder head flow characteristics are the major defining factor in producing top end</u> <u>power</u> with this combo and that until the cylinder heads are extensively ported to create higher flow, the other intake and exhaust system changes will remain insignificant.

For a street/strip engine, the current combo with the dual plane manifold seems unbeatable with between 550 and 610 ft-lbs of torque from 3000 rpm to 5500 rpm and 575 hp at 5700 rpm. However, the goal for this project is to run 9.9s on the motor which requires about 15% more power from the engine (640-660 hp). John lingenfelter's 502 testing shows on a very similar engine combo with his slightly bigger cam and his smaller heads produced 665 hp at 6500 rpm with only 9.2:1 compression. With our 10.5:1 compression, bigger heads (290cc vs 264cc), bigger Dart single plane intake (extrude honed), bigger and better exhaust headers (2-1/8" vs 2"), we should be able to meet or exceed his 665 hp using our smaller cam (246/246 vs 260/268).

Also, Comp Cams states that the hp peak for the current cam is 6500-6800 rpm and this combo tested out to a 5700-5900 rpm hp peak – again showing significant top end breathing restrictions.

Conclusions

We took a great deal of time and effort to build up a highly reliable killer street/strip motor and made only one mistake – we pulled a set of stock aftermarket aluminum heads out of the box and bolted them on without any porting work. This in conjunction with a 1/8" port mismatch on the top and bottom of the intake runners going into a smaller head port is the most likely cause of the loss in top end power.

The heads need to be carefully machined to port match them to the 2 different intake manifolds, open up the intake runners, perform careful bowl blending work, check valve seat angles, etc. in order to get them to flow 25-30% more at 0.500-0.650" lift to meet our 640-660 hp goal with the current mild solid roller cam. The ideal result would be to get to 640-650 hp with the extrude hone ported Edelbrock Performer RPM dual plane manifold and 660-680 hp with the extrude hone ported Dart single plane manifold. It is acceptable to raise the intake port height to create more of a rectangular port shape (both the heads and manifolds) if so required.

Reaching the power targets noted above may require a change in cams and carbs and therefore a larger roller cam (264/264 vs. 246/246) and a 1050 Dominator carb will be tested on the dyno as well as the existing setup.

Here are the next set of dyno run tests to be performed after the heads are re-worked:

- 1.Dual plane intake with 246/246 @ 0.050" 0.623" lift cam, 110 spacing
- 2.Same setup with dominator (if air flow indicates a need for more carb)
- 3.Single plane intake with same cam and smaller carb
- 4.Same setup with dominator
- 5.Change to new cam with 264/264 0.651" lift, 110 spacing (if needed to meet power goals)

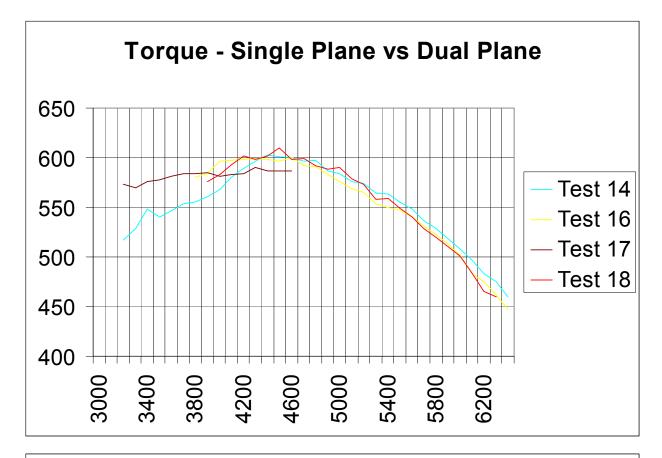
Engine Specifications

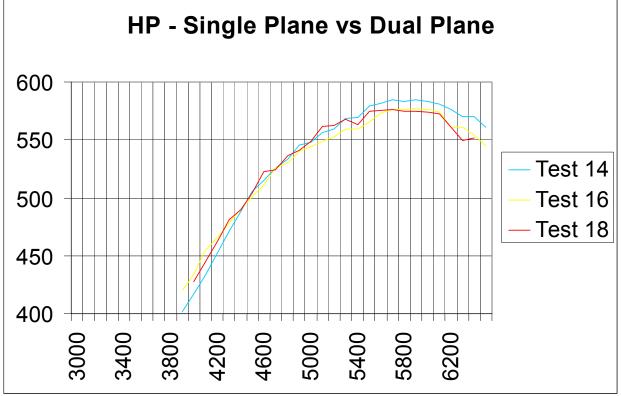
BB Chevy - 502CID, Mark VI (that's right, the new block) Comp Cams 288AR cam with K11-692-8 K-kit Comp Cams Hi-tech solid roller lifters, springs and retainers (as per above) Comp Cams Hi-tech rocker arms Comp Cams stud girdles Comp Cams Hi-tech push rods Stock forged cranked, balanced Fluidamper Mallory H beam rods JE pistons, 10.5:1, JE gapless rings Edelbrock Performer RPM heads, Oval Port, 290cc intakes, 100cc exhausts, 110cc chamber 2.19/1.88 valves with 11/32" valve stems Dart oval port single plane intake, extrude hone ported – option A Edelbrock Performer RPM oval port dual plane intake, extrude hone ported – option B Carb Shop double pumper 750 – massaged to 930cfm – option A 1050 CFM dominator carb – option B 2-1/8 x 32 Jerry Stahl headers, 3-1/2 x 15 collectors (Borla X-1 mufflers optional) NOS fogger direct port injection system tuned for 300hp, PWM electronic control MSD 6AL ignition, MSD billet distributor Taylor 10mm wires

Drivetrain

TH-400 Transmission, 3500rpm stall converter, no trans-brake

Strange 9" rear assembly, 3.70 or 3.89 gears driving 10x28" slicks, Wilwood rear disk brakes 3400lbs car, AVO coil-overs in rear, adjustable trailing links, adjustable mounting points





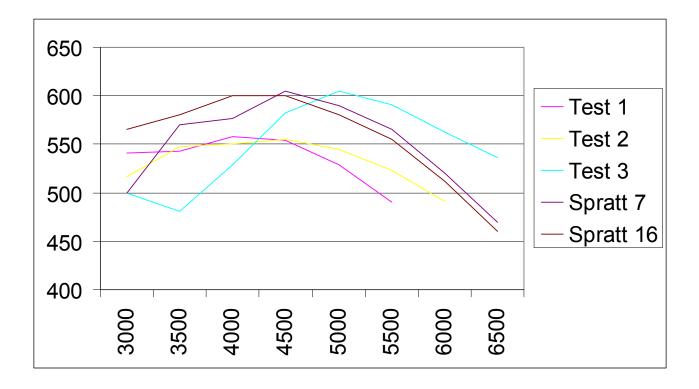
Test 1 is the Lingenfelter 502 setup (9.2:1 CR) with a mild 210/218 hydraulic cam, Edelbrock Performer dual plane manifold, 4779 750cfm double pumper carb, and 224cc "peanut" truck heads

Test 2 is the Lingenfelter 502 setup with a more aggressive 236/236 - 0.556" hydraulic cam, Edelbrock Performer RPM dual plane manifold and 264cc oval port heads (2.25/1.88 valves)

Test 3 is the same setup as above with a 260/268 - 0.714" solid roller cam, Dart single plane manifold, and 1050 Dominator carb

Spratt 7 is our best extrude honed Dart single plane manifold pull

Spratt 16 is our best extrude honed Edelbrock Performer RPM dual plane manifold pull with some compensation added in for the loss in power on day 2 (5-10ft-lbs added back in to match Day 1 results test #7 with day 2 benchmark run #14).



Appendix A – Dyno Results

<u>Test #2 – first full pull, initial setup: Dart single plane manifold, carb shop 4779 double pumper</u> @ 926cfm with 72/82 jets, 33 degrees total timing/16 initial, 1" spacer (May 15/97)

- Noticed loud exhaust ticking sound immediately after pull, did not locate source for the remainder of the day.
- Found out at the start of day 2 that the #4 exhaust port had blown out the head gasket due to a poor seal of the header at the back of the engine.
- The #4 spark plug had also worked itself loose during the day.
- Finally, the coil to distributor high voltage wire had worked itself loose and had marginally damaged the distributor cap contacts (possible loose of voltage to the plugs for the remainder of day 2?)
- Uneven temperature of the intake air and quality of the air was also an initial potential problem due to burning oil in the exhaust system from prior use with a failed engine on the dyno

LData from computer disk file - (DEREK2)

| Sta | ndard C | orrecta | ed Data | a for a | 29.92 | inches | s Hp. | 60'F dry | air | | Test# | |
|---------------|---------|---------|---------|-------------|-------|---------|--------|----------|-----------|--|---------------------|--------|
| Vapor | Pressur | e: .33 | 3 | | Baro | astric | Pres. | | 21 | Rat | Sensor: io: 1.20 | TO 1 |
| cogine | Турез | 4-cyer(| a pbeur | < | Lngı | ne disp | olace# | ent: 502 | . 10 | 対なかり | ske: 4. | 212191 |
| RFM | CBT | CEHP | EPD | VEX | ME% | FА∻FВ | AL | AZE | 997C | CAT | DIL WAT | BSAC |
| | Lb-Ft | | | | | Lb/Hr | scřm | | | for the second s | Out Out | |
| 3800 | 567.6 | 410.7 | 74.3 | 97.2 | 84.i | 179.5 | SØ2.0 | 12.8 | . 46 | 92 | Ø 175 | U. 86 |
| 3900 | 564.9 | 419.5 | . 77.7 | 96.8 | 83.8 | 183.6 | 512.9 | 12.8 | .46 | 92 | 0 175 | 5.87 |
| 4000 | 563.2 | 428.9 | 81.3 | 99.3 | 83.5 | 181.8 | 539.0 | 13.6 | a dip dip | 92 | 0 175 | |
| 41.010 | 571.4 | 446.1 | 84,9 | 99.4 | 83.4 | 181.4 | 353.3 | 14.0 | . 43 | 92 | 0 175 | 5.95 |
| 4200 | 578.3 | 462.5 | 88.5 | 97.9 | 83.3 | 182.7 | 558.1 | 14.0 | . 41 | 92 | Ø 175 | 5.79 |
| 4300 | 589.3 | 482.5 | 93. 3 | 101.0 | 83.3 | 194.2 | 589.4 | 13.9 | . 4£2 | 98 | 0 175 | 5.86 |
| 4400 | 593.4 | 497.1 | 96.1 | 101.9 | 83.2 | 202. Q | 609.1 | 13.8 | . 48 | 92 | 0 175 | 5.80 |
| 4500 | 600.4 | 514.4 | 166.0 | 102.6 | 83.1 | 208.3 | 626.6 | 13.8 | . 42 | 92 | 0 175 | S. 85 |
| 45 M Ø | 592.5 | 518.9 | 104.0 | 99.7 | 82.7 | 215.0 | 622.9 | 13.8 | a di di | 92 | Ø 175 | 5.76 |
| 4700 | 601.3 | 538.1 | 108.0 | 104.1 | 82.6 | 219.3 | 664.4 | 13.9 | . 43 | 승을 | 0 175 | 5.93 |
| 4800 | 599.3 | 547.7 | 112.1 | 103.0 | 82.4 | 226.1 | 672.4 | 13.7 | .43 | 9 î (| 0 175 | 5.69 |
| 4900 | 597.6 | 557.5 | 116.4 | 102.2 | 82.1 | 232.7 | 681.1 | 13.4 | . 44 | 9 i | Ø 175 | 5.87 |
| 5000 | 593.2 | 564.7 | 120.6 | 104.5 | 81.7 | 231. Z | 710.5 | 14. i | . 43 | 91 | Ø 172 | 6.04 |
| 5190 | 584.3 | 567.4 | 125.1 | 124.4 | ε.18 | 244.0 | 724+1 | 13.6 | . 45 | 91 | @ 175 | 6.13 |
| 5200 | 578.9 | 573. e | 129.5 | 103.0 | 80.9 | 24i.8 | 727.8 | 13.8 | . 44 | 91 | Ø 175 | 6.10 |
| 5300 | 570.6 | 375.8 | 134.5 | 102.6 | 80.3 | 250.6 | 739.2 | 13.5 | . 46 | ') 1 | Ø 175 | 6.17 |
| 5480 | 564.9 | 580.8 | 140. i | iØ4.∂ | 79.8 | 254.6 | 764.9 | 13.8 | - 46 | 9i | Ø 175 | 6.33 |
| 5500 | 559.4 | 585.8 | | | | 259.9 | | 13.6 | . 46 | - 91 | Ø 175 | 6.31 |
| 5602 | 551.2 | 587.7 | | | | 261.3 | | 13.7 | . 47 | 91 | Ø 175 | 6.39 |
| 5700 | 543.9 | 590.3 | 157.7 | 99. O | 78.1 | 266.3 | 773.5 | 13.3 | . 47 | 91 | 0 175 | 6.31 |
| 2880 | 533.9 | 589.6 | 163.9 | 100.5 | 77.4 | 268.7 | 793.1 | 13.6 | . 48 | 91 | Ø 175 | 6.48 |
| 5900 | 526.0 | 390. 9 | 170.0 | 96.3 | 76.8 | 263.6 | 772.2 | 13.5 | . 47 | 91 | Ø 176 | 6.29 |
| 6000 | 516.2 | 589.7 | 176.4 | 96.8 | 76.1 | 276.5 | 791.4 | 13.1 | . 49 | 90 | Ø 176 | 6.46 |
| 6100 | 499.0 | 579.6 | 184.8 | 96.2 | 75.0 | 273.8 | 799.4 | t3.4 | . 30 | 90 | 0 175 | 6,64 |
| 6200 | 489.7 | 578.1 | 191.7 | 97.2 | 74.2 | 272.1 | 821.3 | 13.9 | , 49 | 90 | 0 175 | 6.85 |

<u>Test #3 – same setup as #2 (May 15/97)</u>

Data from computer disk file - (DEREK3)

| Sta | Standard Corrected Data for | | | | | inche | 5 Hg. (| 50 F d | ry air | | Test | 科 | З |
|--------|-----------------------------|---------|---------|---------------|--------|--------|---------|----------|-------------|--------|-------------------------|-------|---------|
| Test: | 300 RPI | M/Sec P | lcceler | ation | Fuel | Spec. | Grav. | 4 | .721 | Air | Sens | o mia | 今,② |
| | Pressur | | | | Barros | aetric | Pres. | р 6 \ | 0.01 | Rat: | io: 1 | . ØØ | TO 1 |
| Engine | Type: | 4-Cycle | s Sparl | < · · | Engin | he dis | slacem | ent: S | Ø2.0 | Str | sike : | 4.1 | 3121121 |
| | | | | | | | | | | | | | |
| RPH | CBT | CBHP | PHP | VE% | MEX | FA+FB | Ai | A/F | BSFC | CAT | OIL | WAT | BSAC |
| | Lb-Ft | | | | | L.b/Hr | scfm | | | F | Out | Out | |
| 3800 | 552. 3 | 399.6 | 74.3 | 97.3 | 83.7 | 180.8 | 504.i | 12. | 8.47 | 90 | \otimes | 173 | 6.85 |
| 3900 | 544.6 | 404.4 | 77.7 | 96.6 | 83.3 | 178.2 | 513.2 | 13. | 2.46 | 912 | 1¢1 | 173 | 6.08 |
| 4000 | 557.5 | 424.6 | 81.3 | 97.8 | 83.3 | 181.8 | 532.9 | 13. | 5.45 | 90 | Ø | 173 | 6.02 |
| 4100 | 554,7 | 433.0 | 84.9 | 96 . 4 | 83.0 | 187.2 | 539.7 | 13. | 2 .45 | 68 | Q1 | 173 | 5.97 |
| 4200 | 572.4 | 437.7 | 8a.S | 97.7 | 83.2 | 192.8 | 560.1 | 13. | 3 . 44 | 89 | Ø | 173 | 5.86 |
| 4300 | 380.6 | 475.4 | 92.3 | 100.1 | 83.8 | 202.3 | \$87.9 | 13. | 3 .44 | (3, 2) | 21 | 173 | 5.92 |
| 4400 | 582.2 | 487.8 | 96.i | 103.8 | 82.9 | 209.9 | 623.9 | 13. | 6 .45 | 89 | \otimes | 173 | 6.13 |
| 4500 | 592.8 | 507.9 | 100.0 | 102.l | 82.9 | 218.8 | 626.4 | 13. | 1 .45 | 90 | (Ž) | 173 | 5.91 |
| 4600 | 581.5 | 509.3 | 104.0 | 103.5 | 82.4 | 225.7 | 648.6 | 13. | 2.46 | 90 | Ø | i73 | 6.11 |
| 471210 | 594.5 | 532.0 | 108.0 | 103.8 | 82.5 | 232.4 | 665.3 | 13. | 1 .46 | 90 | Ø | 173 | 6.1212 |
| 4800 | 586.5 | 536.0 | 112.1 | 103.2 | 82.i | 239.8 | 674.8 | 10. | | 90 | ίŽί | 173 | 6.04 |
| 4900 | 582.2 | 543.2 | 116.4 | 104.9 | 81.7 | 248.4 | 700.7 | 13. | 4 .46 | 0 Ø | Ø | 173 | 6.19 |
| 5000 | 582.8 | 554.8 | 120.6 | 103.4 | 81.5 | 245.9 | 704.2 | 13. | 1 .46 | 90 | Ø | 173 | 6.09 |
| 5199 | 571.5 | 555.0 | 125.1 | 102.5 | 30.9 | 254.5 | 711.9 | 12. | 8 .48 | 90 | Ø | 173 | 6.16 |
| 5200 | 567.3 | 561.7 | 129.5 | 103.4 | 80,6 | 256.0 | 732.7 | 13. | 1.48 | 9Ø | 2 | 173 | 5.26 |
| 古道のの | 561.3 | 566.4 | 134.5 | 184.4 | 80.1 | 260.2 | 755.5 | 13. | 3 .48 | 89 | \mathcal{D} | 173 | 6.40 |
| 5400 | 549.3 | 564.8 | 140.1 | 101.7 | 79.4 | 270.2 | 749.7 | iê. | 7 .50 | 89 | Ø | 173 | 6.37 |
| 5500 | 541.7 | 567.3 | 145.9 | 102.6 | 78.0 | 278.7 | 771.1 | 13. | 0.50 | 88 | $\langle 0 \rangle$ | 173 | 6.52 |
| 5600 | 537.8 | 573.4 | 151.7 | 101.6 | 78.3 | 273.2 | 777.9 | 1.3. | 1.50 | 88 | Ø | 173 | 6.50 |
| 5700 | 528.8 | 573.9 | 137.7 | 102.0 | 77.7 | 260.9 | 795.1 | 13. | va "Si | 99 | Ø | 173 | 6.63 |
| 5800 | 518.6 | 572.7 | 163.9 | 101.0 | 77.0 | 281.6 | 800. i | 13. | 0.51 | 88 | Ø | 173 | 6.70 |
| 5900 | 511.4 | 574.5 | 170.0 | 1901.1 | 76.4 | 281.8 | 809.1 | 13. | 2.51 | 87 | 121 | 174 | 6.75 |
| 6000 | 496.9 | 567.7 | 176.4 | 100.5 | 75.5 | 280.9 | 826.2 | 13. | 15 - 15 (S) | 87 | Ø | 174 | 6.98 |
| 6100 | 491.5 | 570.9 | 184.0 | 98.5 | 74.8 | 284.7 | 822.7 | 13. | 3 .52 | 87 | \mathcal{A}^{\dagger} | 174 | 6.92 |
| 6200 | 477.2 | 563.3 | 191.7 | 96.0 | 73.7 | 274.0 | 814.6 | 13. | 7 .51 | 87 | Ø | 174 | 6.94 |
| 6380 | 463.2 | 555.6 | 199.6 | 95.5 | 72.7 | 268.7 | 824.7 | 法保证 | 1 .51 | 87 | ųž) | 174 | 7.13 |
| 6400 | 448.7 | 546.8 | 207.6 | 95.4 | 71.5 | 286.9 | 836.4 | 13. | 4 .55 | 87 | Ø | 174 | 7.36 |

<u>Test #5 – richen jets from 72/82 to 74/84 (May 15/97)</u>

Data from computer disk file - (DEREKS)

| Star | ndard (| Correcte | d Data | a for a | 29 . 92 | inche | s Hg. | 60 F dry | air | | Test | 5 41 | 5 |
|---------|---------|----------|---------|----------|----------------|---------|--------|----------|---------|------|-------------|------|-------|
| Test: | 300 RI | PM/Sec 4 | lccele | ation | Fuel | Spec. | Grav. | ž "7 | 21 | Air | Sen | sori | 9.0 |
| Vapor F | | | | | | wetric | | | | Rati | io: : | 1.00 | 10 1 |
| Engine | Type: | 4-Cycle | : Sparl | ∢ | Engi | ne dis; | placem | ent: 502 | \$ Ø | Stro | oke: | 4.4 | 12021 |
| MGH | CBT | CBHP | FHP | VE% | MEX | SA+FB | A1 | A/F | BSFC | CAT | OIL | WAT | BSAD |
| | Lb-Ft | | | | | Lb/Hr | scfm | | | 2 | Out | Out | |
| 3800 | 569.4 | 412.0 | 74.3 | 96.1 | 84.2 | 175.0 | 499.8 | 13.1 | . 44 | 87 | Ø | 171 | S. 79 |
| 3900 | 564.4 | 419.1 | 77.7 | 97.7 | 83.8 | 176.8 | 521.9 | 13.6 | , 44 Ap | 87 | Ø | 173 | 5.95 |
| 4000 | 565.6 | 430.8 | 81.3 | 96.2 | 83.6 | 184.3 | 525.8 | 13.1 | . 45 | 88 | Ø | 173 | 5.84 |
| 4100 | 368.9 | 444.1 | 84.9 | 95.6 | 83.4 | 182.9 | 535.8 | 13.5 | . 4.3 | 88 | \otimes | 173 | 5.77 |
| 4200 | 593.5 | 474.6 | 88.5 | 99.3 | 83.7 | 192.2 | 569,5 | 13.6 | . 42 | 88 | Ø | 173 | 5.74 |
| 4300 | 600.9 | 492.0 | 98. 3 | 101.3 | 83.6 | 205.4 | 594.7 | 13.3 | 。存存 | 89 | Ø | 173 | 5.79 |
| 44210 | 602.7 | 524.9 | 96.1 | 102.0 | 83.4 | 207.5 | 613.0 | 13.6 | ,43 | 89 | Q. | 173 | 5.8: |
| 4300 | 607.6 | 520.6 | 100.0 | 101.0 | 83.3 | 213.8 | 619.5 | 13.3 | . 43 | 89 | Ø | 173 | 5.70 |
| 4600 | 607.8 | 532.3 | 104.0 | 102.3 | 83. i | 223.5 | 643.7 | 13.8 | * 444 | 88 | Ø | 173 | 5.76 |
| 4720 | 601.2 | 538.0 | 108.0 | 103.1 | 82.7 | 326.5 | 661.9 | 13.4 | . 44 | 88 | 12 | 173 | 5.89 |
| 48243 | 604.6 | 552.6 | 112.1 | 102.6 | 82.5 | 236.0 | 672.7 | 13.1 | . 45 | 88 | Ø | 173 | 5.80 |
| 4900 | 595.6 | 555.7 | 116.4 | 101.2 | 82.1 | 236.9 | 677.7 | 13.1 | , la la | 88 | Ø | 173 | 5.84 |
| 5000 | 594.1 | 565.6 | 120.6 | 102.8 | 81.8 | 244.6 | 702.3 | 13.2 | . 45 | 88 | Ø | 173 | 3.94 |
| 5100 | 587.1 | 570.1 | 125.1 | 103.4 | 81.4 | 237.6 | 721.0 | 13.9 | . 43 | 88 | <i>\$</i> 3 | 173 | 6.0 |
| 5200 | 583.9 | 578.1 | 129.5 | 104.6 | 81.1 | 245.5 | 744.9 | 13.9 | " 444 | 87 | Ø | 173 | 6.18 |
| 5300 | 574.0 | 579.2 | 134.5 | 101.6 | 80.5 | 251.4 | 737.4 | 13.5 | . 45 | 87 | Ø | 173 | 6.09 |
| 5400 | 569.7 | 585.8 | 140.1 | 102.9 | 80.0 | 258.9 | 761.1 | 13.5 | . 46 | 87 | Ø | 173 | 6.22 |
| 5300 | 560.5 | 587.0 | 145.9 | 102.0 | 79.4 | 275.7 | 768.2 | 12.7 | . 49 | 87 | Ø | 173 | 6.26 |
| 5600 | 555.0 | 591.8 | 151.7 | 99. S | 78.9 | 271.5 | 760.4 | 18.9 | . 48 | 87 | Ø | 173 | 6.13 |
| 5700 | 544.6 | 591.1 | 157.7 | 100.2 | 78.2 | 273.Ø | 782.1 | 13.2 | - 48 | 87 | Ø | 173 | 6.34 |
| 5800 | 538.4 | 594.6 | 163.9 | 97.6 | 77.7 | 273.0 | 775.3 | 13.0 | . 48 | 87 | Ø | 175 | 6.23 |
| 3900 | 529.1 | 594.4 | 170.0 | 96.1 | 77.0 | 279.7 | 776.2 | 12.7 | . 49 | 37 | Ω. | 175 | 6.26 |
| 61262 | 519.4 | 593.4 | 176.4 | 96.0 | 76.3 | 274.7 | 788.5 | | . 48 | 87 | Ø | 175 | 6.37 |
| 6100 | 506.2 | 587.9 | 184.0 | 95.0 | 75.4 | 259.9 | 794.1 | 14.0 | . 46 | 87 | 1Z | 176 | 6.48 |
| 6200 | 496.9 | 586.6 | 191.7 | 95. Ø | 74.5 | 271.4 | 807.1 | 13.7 | . 48 | 87 | | 175 | 6.62 |
| 6300 | 490.2 | 588.0 | 199.6 | 95.9 | 73.8 | 280.5 | 827.1 | 13.5 | . 50 | 87 | <i>©</i> 1 | 175 | 6.75 |
| 6412102 | 473.2 | 576.6 | 207.6 | 94.7 | 72.6 | 264.6 | 830.1 | 1 4 . 4 | . 48 | 87 | | 175 | 6.92 |

<u>Test #6 – richen jets from 74/84 to 76/88 (May 15/97)</u>

Data from computer disk file - (DEREK7)

| Sta | ndard (| lorrecte | d Data | a for a | 29.92 | inches | s Hg. I | 60 F dr | y air | | Test | ;排 : | 6 |
|-----------------|---------|--------------|--------|---------|-------|---------|---------|----------|---------------|----------|------------|--------------|--------------|
| Test: | | M/Sec A | | ration | | ' | | | 721 | | Sens | | |
| Vapor i | | | | | | setric | | | <u>.</u> ki i | | | | íU 1 |
| Engine | Type: | 4-Cycle | Sparl | < | Engir | ne disp | olacem | ent: 50 | 2.0 | Stru | oke: | 4,6 | 9/21/2 |
| RPM | CBT | СВНР | FHP | VEX | 州三% | FA+FB | A1 | A/F | BSEC | | | | BSAC |
| 175 275 275 275 | Lb-Ft | ب اندار و در | | | | Lb/Hr | scfm | 1 **** # | · | F | Out | Out | 5.87 |
| 3800 | 574.0 | 415.3 | 74.3 | | 84.3 | | 508.8 | 13.4 | | 90 60 | 2 12 | $174 \\ 174$ | 5.94 |
| 3900 | 563.2 | 418.2 | 77.7 | | | 185.1 | 517.9 | 12.8 | | 90 | | 174 | 5.82 |
| 4000 | 571.9 | 435.6 | 81.3 | | | 189.3 | | 12.8 | | 90 | Ø Ø | | 3.82 5.79 |
| 4100 | 581.9 | 454.3 | 84.9 | | | 199.4 | | 12.6 | | 90 | ••• | | 5.66 |
| 4200 | 585.7 | 468.4 | 88.S | | | 202.8 | | 18.5 | | 90 | 24 24 | 174 | 5.70 |
| 4300 | 602.8 | 493.5 | 92.3 | | | 217.0 | | 12.4 | | 90 | | 174 | 5.81 |
| 4400 4500 | 603.6 | 505.7 | 96.1 | | | 219.9 | | 12.8 | | 90 50 | ų A | 174 | 5.81 5.83 |
| 4500 | 608.i | | 100.0 | | | 229.5 | | | | 90 | 0 - 01 | | 5.93 |
| 46ØØ | 607.3 | | | | | 234.4 | | | | 90 90 | 21 (21 | | 5.89 |
| 4700 | 602.8 | | | | | 238.5 | | 12.8 | | 90 90 | en Ø | 173 | 5.91 |
| 4800 | 600.2 | | | | | 247.8 | | 18.5 | | | 121 121 | | |
| 4900 | 591.i | | | | | 248.2 | | | | 90 90 | | 173 | 6.Ø1 |
| 5000 | 594.0 | | | | | 248.7 | | 13.1 | | | Ø | 173 | 6.00 5.95 |
| 5100 | 586.7 | 569.7 | | | | | | 12,8 | | 90 | | 173 | |
| 5200 | 578.9 | 573.2 | | | | 255.8 | | 13.0 | | 9位 5つ | | | 6.06 |
| 5300 | 573.e | 578.4 | | | | 262.1 | | 13.2 | | 9Ø | | 173 | 6.25 |
| 5400 | 567.2 | 583.2 | | | | 278.4 | | 12.5 | | 90 | Ø | 173 | 6.26 |
| 5500 | 553.9 | | 145.9 | | | 280.9 | | 12.3 | | 90 | 12 | 174 | 6.24 |
| 5600 | 551.0 | | 151.7 | | | 283,4 | | 12.7 | | 90 | Ø | 174 | 6.41 |
| 5700 | 543.8 | 590.2 | | | | 278.4 | | 12.7 | | 90 | ø | | 6.27 |
| 5800 | 535.6 | | 163.9 | | | 279.7 | | 12.0 | | 89 | Ø | 174 | 6.35 |
| 5900 | 527.i | | 170.0 | | | 278.6 | | 13.3 | | 89 | Ø | 174 | 6.53 |
| 6000 | 515.1 | | 176.4 | | 76.1 | | | | | 66 | 121 | 174 | 6.57 |
| 6100 | 504.3 | 585.7 | | | | 276.7 | | 13.2 | | 89 | Ø | 174 | 6.53 |
| 6220 | 490.0 | 579.4 | | | | 288.4 | | 13.0 | | 89 | Ø | | 6.78 |
| 6300 | 482.1 | 578.3 | | | | 268.9 | | 14. 2 | | 89 | | 174 | 6.94 |
| 6400 | 474.4 | 578.1 | 897.6 | 93.8 | 12.6 | 278.6 | 819.9 | 13.5 | .51 | 89 | Ø | 174 | 6.83 |

Test #7 – advance timing from 33 to 36 degrees (May 15/97)

Data from computer disk file - (DEREK8)

| | | | | | | | | ŵ F dry | | | | 7 |
|--------|---------|---------|---------|-------|-------|---------|----------------|---------|--------------|-----|---------|---------|
| | | | | | | | | . Z | | | | ·: 9.Ø |
| Vapor | Pressur | ·e: .3: | 3 | | Baro | netric | Pres. 1 | 30. | 21 | Rat | io: 1.0 | NØ TO 1 |
| Engine | Type: | 4-Cycle | 3 Spar) | < | Engin | ne disp | olaceme | nt: 502 | . Ø | Str | oke: Z | 1. ØØ¢ |
| | | | | | | | | | | | | |
| RPM | CBT | CBHP | 行居住 | VE% | MEX | | 61 | | BSFC | | OIL WA | |
| | Lb-Ft | | | | | | scfm | | | | Out Ou | |
| 3800 | 579.5 | 419.3 | | | | | 503.2 | 12.3 | | | | |
| 3900 | 568.2 | 421.9 | | | | | 508.2 | 12.4 | | | 0 17 | |
| 4000 | 576.5 | 439.1 | | | | 195.5 | | 13,0 | | | 0 17 | |
| 4100 | 580.1 | 452.9 | | | | | 547.0 | 13.0 | , de la | | | |
| 42/202 | 396.6 | 477.1 | | | | | 570.0 | 12.9 | . 44 | | | |
| 4300 | 603.Ø | | | | | | 589.6 | 12.8 | a XP ST | | | |
| 4400 | 595.9 | | | | | | 594.7 | | . Ap Ap | | | |
| 4500 | 596.8 | | | | | | 622.0 | 12.7 | . 46 | | | |
| 46000 | 605.4 | | | | | | 650.0 | 液色,9 | . 46 | | | |
| 4700 | 601.7 | | | | | 232.9 | | 13.1 | , 4 <u>5</u> | | | |
| 48家母 | 601.5 | | | | | | 680.4 | 13.0 | .46 | | | |
| 4900 | 603.6 | | | | | | 687.2 | 12.8 | . 4b | | | |
| 5000 | 589.3 | | | | | 24i.8 | 1.48 | 13.2 | .45 | | | |
| 5100 | 588.3 | | | | | 255.5 | | 13.2 | . 47 | | | |
| 5220 | 583.5 | | | | | 264.6 | | 12.9 | 。4日 | | | |
| 5300 | 578.5 | | | | | 270.0 | | 12.8 | . 48 | | | |
| 5400 | 570.0 | | | | | 277.5 | | 12.5 | . 49 | | | |
| 5500 | 558.0 | | | | | 271.6 | | 12.7 | . 49 | | | |
| 5600 | 557.6 | 594.5 | 151.7 | 99.7 | 78.9 | 290.7 | 762.1 | 12.0 | . 51 | | | |
| 5700 | 544.1 | 590.5 | 157.7 | 100.9 | 78.2 | 286.1 | 784.6 | 12.6 | .51 | 89 | Ø 17 | 8 6.3 |
| 5800 | 537.4 | 593.5 | 163.9 | 98.2 | 77.8 | 278.6 | 777.9 | 12.8 | . 49 | 69 | | |
| 5900 | 523.9 | 588.5 | 170.0 | 99. Ø | 76.8 | 290.8 | 797.8 | 12.6 | , 52 | 89 | Ø 17 | '8 6.S |
| 6000 | 517.9 | 591.7 | 176.4 | 97.4 | 76.2 | 269.6 | 79 8 .Ø | 13.6 | . 4B | | | |
| 6100 | 504.6 | 586.i | 184.0 | 95.2 | 75.3 | 280.4 | 792.6 | 13.0 | .50 | 89 | 017 | 'a 6.5 |
| 6200 | 502.2 | | | | | | 805.4 | 13.4 | . 49 | eв | | |
| 6300 | 484.9 | 581.7 | 199.6 | 94.1 | 73.5 | 276.8 | 809.9 | 13.4 | .50 | 68 | Ø 17 | 6.7 |
| 6400 | 474.2 | 577.9 | 207.6 | 93.5 | 7E.6 | 294.5 | 817.2 | 12.7 | - 33 | 89 | 0 17 | 18 6.8 |

Test #8 – add 18" exhaust reducer/extensions (May 15/97)

Data from computer disk file - (DEREK9)

| Sta | ndard | Correcte | ed Data | a for i | 29.92 | inche | s Hg. | 60 F | dry air | | Test | : 朴 | - 6 |
|--------------------------|--------------|--------------------------------|---------|---------|---------|----------------|------------|------|------------------------|----------|-----------------------|-----|------------|
| Test: Vapor Engine | Pressu | PM/Sec A re: .33 4-Cycl: | 3 | | Baro | netric | Pres. | 3 | .721 30.02 502.0 | Rat | Sens lo: : ske: | | TO 1 |
| RPM | CBT L5-Ft | СВНР | FHP | VEX | ME% | FA4FB Lb/Hr | Al scfm | Α/ | F BSFC | CAT F | OIL Out | | BSAC |
| 3800 | 591.9 | 428.3 | 74.3 | 60 S | ឆ្នេ ឆ្ | 193.4 | | | .3.47 | | | 173 | 5.74 |
| 3900 | 580.9 | | 77.7 | | | 190.6 | | | | 83 | | 174 | 5.86 |
| 4000 | 577.1 | | 81.3 | | | 198.5 | | | | | | 174 | 5.85 |
| 4100 | 577.3 | | 84.9 | | | 200.9 | | | | | | 174 | 5.74 |
| 4200 | 584.4 | | 88.5 | | | 199.8 | | | .944 | | | 174 | 5.71 |
| 4300 | 584.4 | | 98.3 | | | 217.9 | | | | | ä | | 5.70 |
| 44ØØ | 591.1 | | 96.1 | | | 215.0 | | | | | i2 | 174 | 5.62 |
| 4500 | 590.4 | | 100.0 | | | 217.6 | | | | | ő | | 5.74 |
| 4620 | 386.Ø | 513.3 | 104.0 | 98.2 | 82.7 | 226.5 | 624.4 | 12 | . 7 . 46 | 38 | 173 | 174 | 5.78 |
| 4780 | 591.0 | | 108.Ø | 99.9 | 82.5 | 229.7 | 649.4 | 13 | .0 .45 | 82 | 0 | 174 | 5.83 |
| 4800 | 586.8 | 536 J | 112.1 | 102.2 | 32.2 | 240.7 | 678.7 | 18 | . 9 . 46 | 82 | Ø | 174 | 6. Ø1 |
| 4900 | 586.1 | 546.8 | 116.4 | 99. j | 81.9 | 246.4 | 671.4 | 12 | .5.47 | 82 | Ø | 174 | 5.83 |
| 5000 | 584.6 | 336.3 | 120.6 | 98.2 | 81.7 | 242.1 | 679.4 | 12 | .945 | 88 | 8 | 174 | 5.00 |
| 5100 | 577.7 | 561.0 | 125.1 | 98.9 | 81.2 | 248.5 | 697.6 | 12 | .9.46 | 82 | Ø | 174 | 5.91 |
| 5200 | 573.7 | | 129.5 | | | 260.4 | | | .7.47 | 88 | Ø | 174 | S.Ø5 |
| 5300 | 568.5 | | 134.5 | | | 264.3 | | | .8 .48 | -82 | Ø | 174 | 6.11 |
| 5400 | 360.3 | | 140.1 | | | 278.6 | | | .4 .50 | 28 | 2 | 175 | 6.19 |
| 5500 | 557.6 | | 145.9 | | | 275.3 | | | | | | 175 | 5.33 |
| 5600 | 552.7 | | 151.7 | | | 287.7 | | | | 82 | | 175 | 6.27 |
| 5700 | 543.2 | | 157.7 | | | 273.3 | | | | | | 176 | 6.38 |
| 5800 | 529.5 | | 163.9 | | | 280.3 | | | | | | 176 | 6.45 |
| 5900 | 522.8 | | | 98.5 | | 285.6 | | | | 82 | | 176 | 6.52 |
| 6000 | 510.5 | | | | | 291.2 | | | | | | 176 | 6.58 |
| 6100 | 496.1 | 576.2 | | | | 270.3 | | | | 88 | Ø | 176 | 6.71 |
| 6200 | 487.7 | | | | | 294.2 | | | | | 121 | 176 | 6.65 |
| 6300 | 480.9 | | | | | 276.0 | | | | 83 | Ø | 176 | 6.71 |
| 64回回 | 469.6 | 572. <i>2</i> | 241.0 | 98.1 | 12.6 | 271.5 | 813.2 | 13 | . 6 . 49 | 83 | Ø | 176 | 6.79 |

<u>Test #9 – change to 2" spacer (May 15/97)</u>

Data from computer disk file - (DEREK10)

| Star | ndard (| Correcte | ed Data | a for a | 29.92 | inche | s Hg. (| 50 F dry | air | | Test | 计 | 9 |
|---------|--------------|----------|---------|---------|-------|----------------|------------|----------|----------------------------|----------|---------------|------------|------|
| Test' | 300 RF | M/Sec A | loceler | ation | Fuel | Spec. | Grav. | | | | | sori | |
| Vapor i | | | | | | netric | | | | Rati | io: | | TO 1 |
| Engine | Туре: | 4-Cycle | e Sparl | 4 | Engin | ne disp | olacem | ent: 502 | . 0 | Stri | ske: | 4.4 | 3696 |
| RPM | CBT Lb-Ft | СВНР | FHP | VEX | MEX | FA+FB Lb/Hr | 日1 scfm | AVE | BSFC | CAT F | | WAT Out | BSAC |
| 3800 | 596.4 | 431.5 | 74.3 | 100.6 | 84.8 | 191.8 | 523.6 | 12.5 | . 46 | 87 | Ø | 170 | 5.79 |
| 3900 | 586.2 | 435.3 | 77.7 | 99.2 | 84.3 | 194.Ø | 529.8 | 12.5 | . 46 | 87 | Ø | 17Ø | 5.81 |
| 4000 | 577.9 | 440.1 | 81.3 | 98.7 | 83.9 | 193.4 | 540.9 | 12.8 | . 46 | 87 | Ø | 170 | 5.86 |
| 4100 | 585.3 | 456.9 | 84.9 | 98.5 | 83.8 | 197.8 | 553.4 | 12.8 | .43 | 87 | Ø | 171 | 5.78 |
| 4200 | 586.9 | 469.3 | 88.5 | 98.9 | 83.6 | 201.4 | 568.9 | 13.0 | .45 | 87 | Ø | 171 | 5.78 |
| 4300 | 582.9 | 477.2 | 92.3 | 100.0 | 83.3 | 203.5 | 588.8 | 13.3 | , 44 | 87 | 12 | 171 | 5.89 |
| 44010 | 589.5 | 493.9 | 96.1 | 100.6 | 83.2 | 209.1 | 606.4 | 13.3 | 44 | 87 | \otimes | 171 | 5.86 |
| 4500 | 592.9 | 508.0 | 100.0 | 101.5 | 83.0 | 209.9 | 625.5 | 13.7 | , 43 | 87 | \mathcal{O} | 171 | 5,88 |
| 46/21/2 | 395.0 | 521.1 | 104.0 | 101.3 | 82.8 | 217.7 | 638.1 | 13.5 | .43 | 87 | \otimes | 171 | 5.84 |
| 4700 | 592.8 | 530.5 | 108.0 | 100.8 | 82.5 | 217.0 | 649.1 | 13.7 | .43 | 87 | Ø | i71 | 5.84 |
| 4800 | 597.6 | 546.2 | LIE.I | 101.9 | B⊇. 4 | 228.8 | 670.l | 13.4 | , 44 | 87 | 0 | 172 | 5.86 |
| 4900 | 584.4 | 545.2 | 116.4 | 101.6 | 81.8 | 241.2 | 683.1 | 13.0 | , 46 | 86 | Ø | 172 | 5.98 |
| 5000 | 582.4 | 554.5 | 120.6 | 105.3 | 81.5 | 237.6 | 721.1 | 13.9 | . 45 | 87 | Ø | 172 | 6.21 |
| 5100 | 586.3 | 569.3 | 125.1 | 104.2 | 81.4 | 246.2 | 730.1 | 13.6 | . 45 | 86 | Ø | 173 | 6.12 |
| 5200 | 869.7 | 564.L | 129.5 | 103.1 | 82.7 | 248.9 | 735.7 | 13.6 | . 46 | 86 | 6 | 173 | 6.22 |
| 5300 | 568.6 | 573.8 | 134.5 | 100.7 | 80.4 | 277.8 | 738.5 | 12.1 | . 50 | 86 | Ø | 173 | 6.09 |
| 5400 | 559.6 | 575.4 | 140.1 | 99.9 | 79.8 | 277.5 | 740.4 | 12.3 | . 50 | 86 | Ø | 173 | 6.14 |
| 5500 | 556.4 | 582.7 | 145.9 | 103.2 | 79.3 | 283.3 | 778.8 | 12.6 | . 51 | 86 | Ø | 173 | 6.38 |
| 5600 | 549.4 | 585.8 | 151.7 | 101.2 | 78.8 | 286.6 | 778.0 | 12.5 | .51 | 88 | Ø | 173 | 6.34 |
| 5700 | 541.4 | 587.6 | 157.7 | 98.5 | 78.2 | 281.4 | 770.5 | 12.6 | . 50 | 86 | Ø | 173 | 6.27 |
| 5800 | 530.2 | 585. 5 | 163.9 | 190.1 | 77.4 | 289.4 | 796.9 | 12.6 | .51 | 86 | Ø | 173 | 6.51 |
| 5900 | 522.8 | 587.3 | 170.0 | 99.7 | 76.8 | 294.1 | 807.2 | 12.6 | . 52 | 86 | Ø | 173 | 6.58 |
| 62100 | 512.1 | 585.0 | 176.4 | 96.2 | 76.1 | 281.4 | 792.3 | 12.9 | 1755 1949 1850 1949 | 86 | Ø | 174 | 5.49 |
| 6100 | 498.9 | 579.5 | 184.0 | 97.6 | 75.1 | 292.3 | 816.8 | 12.8 | . 53 | 86 | Ø | 175 | 6.75 |
| 6500 | 494.0 | 583.2 | 191.7 | 96.2 | 74.4 | 288.9 | 818.8 | 13.0 | .52 | 86 | 应 | 175 | 6.73 |
| 6300 | 480.7 | 576.6 | 199.6 | 94.8 | 73.5 | 277.1 | 820.8 | 13.6 | .50 | 85 | ١Ž) | 175 | 6,82 |
| 6400 | 465.4 | 567.1 | 207.6 | 93.2 | 72.3 | 276.5 | 818.6 | 13.6 | . 51 | 86 | Ø | 175 | 6.92 |

Test #10 - remove exhaust reducer/extensions (May 15/97)

Data from computer disk file - (DEREK11)

| si) ⊱ e(| ngaro u | orrecte | na Dece | а торы | బిహి హింద | inche | s ng. o | Ø F dry | air | | 105 | C 11 | 12 |
|----------|---------|---------|---------|--------|-----------|---------|---------|---------|------------------|-------|---------------|-----------------|------------------|
| fest: | 300 RÞ | M/Sec f | Accele | ration | Fuel | Spec. | Grav.: | . " "7 | 21 | Air | Sen | sort | 9.0 |
| | | ·e: .33 | | | | | | 30. | | | | 1.00 | |
| ingine | Type: | 4-Cycle | • Sparl | < | Engi | ne disp | olaceme | nt: 502 | , Ø | Stro | ske∗ | 4.4 | 900 |
| RPM | CBT | СВНР | FHP | VEX | MEX | FA+FB | A1 | A/F | BSFC | CAT | OIL | WAT | BS |
| | Lb-Ft | | | | | Lb/Hr | scfm | | | lear. | Out | Out | |
| 3800 | 572.9 | 414.5 | 74.3 | 99.9 | 84.3 | 191.3 | 521.9 | 18.5 | "4B | 65 | \mathcal{Q} | 178 | i." Sala |
| 3900 | 563.6 | 418.5 | 77.7 | 96.6 | 83.9 | 190.6 | 519.7 | 12.5 | . 47 | 84 | Ø | 178 | |
| 4000 | 574.1 | 437. E | 81.3 | 96.2 | 83.9 | 191.1 | 530.5 | 12.7 | . 45 | 84 | Ø | 178 | ш. С. |
| 4100 | 590.1 | 460.7 | 84.9 | 97.4 | 84.0 | 199.4 | 550.5 | 12.7 | .45 | 84 | Ø | 178 | ыт Сла |
| 4200 | 596.9 | 477.3 | 88.5 | 100.5 | 83.9 | 203.1 | 582.0 | 13.2 | | 84 | Ø | 1.77 | star Start of |
| 4300 | 600.8 | 491.9 | 92.3 | 100.2 | 83.7 | 208.5 | 594.2 | 13.1 | . 44 | 84 | \otimes | 177 | 53 a |
| 44/21/2 | 604.1 | 506.1 | 96.1 | 103.8 | 83.6 | 210.6 | 629.3 | 13.7 | . 43 | 84 | · Ø | 177 | 3. |
| 4500 | 6Ø2.i | 515.9 | 100.0 | iØ2.1 | 83.3 | 816.4 | 633.6 | 13.4 | . 43 | 84 | Ø | 177 | <u>н</u> 14 |
| 46.00 | 600.7 | 526.1 | 104.0 | 102.8 | 83.0 | 220.1 | 652.0 | 13.6 | . 43 | 84 | Ø | 177 | 5. |
| 4700 | 604.3 | 540.8 | 108.0 | 102.2 | 82.9 | 224.1 | 661.9 | 13.6 | . 43 | 84 | Ø | 177 | PET N |
| 4800 | 602.8 | 550.9 | 112.1 | 101.4 | 82.6 | 231.5 | 669.5 | 13.3 | . 44 | 83 | (Z) | 175 | ية لي يو ليبو |
| 4900 | 592.5 | 552.8 | 116.4 | 103.6 | 82. i | 241.6 | 698.4 | 13.3 | . 45 | 0e | (2) | 176 | 6. |
| 5000 | 588.Ø | 559.8 | 120.6 | 104.2 | 81.7 | 240.5 | 717.1 | 13.7 | .45 | 85 | 2 | 176 | δ., |
| 5100 | 584.5 | 567.6 | 125.1 | 103.7 | 81.4 | 247.0 | 727.6 | 13.5 | . 4 [€] | 85 | 20 | 176 | б. |
| 5200 | 580.4 | 574.7 | 129.5 | 101.6 | 81.0 | 264.4 | 726.7 | 12.5 | . 48 | 85 | ťð | 176 | Ó # |
| 5300 | 569.6 | 574.8 | 134.5 | 103.2 | 80.4 | 274.6 | 752.1 | 12.6 | .50 | 85 | \mathcal{Q} | 176 | 6. |
| 5400 | 563.1 | 579.0 | 140.1 | 102.1 | 79.9 | 275.4 | 758.8 | 12.7 | - 49 | 83 | Ø | 176 | ě. |
| 5500 | 559.5 | 585.9 | 145.9 | 101.7 | 79,4 | 287.8 | 769.6 | iE.3 | . 51 | 85 | Ø | 176 | 6. |
| 5600 | 549.5 | 385.9 | 151.7 | 101.3 | 78.8 | 292.6 | 788.4 | 12.2 | . 52 | 85 | Ŵ | 176 | 6. |
| 5700 | 542.3 | 588.6 | 157.7 | 98.9 | 78.2 | 286.Ø | 775.8 | 12.5 | . 51 | 85 | Ø | 176 | 6. |
| 5800 | 530.8 | 586.2 | 163.9 | 98.0 | 77.5 | 278.5 | 782.0 | 12.9 | . 49 | 85 | Ø | 176 | ٤. |
| 5900 | 521.8 | 586.2 | 170.0 | 98.6 | 76.8 | 270.4 | 800.3 | 13.6 | . 48 | 33 | 10 | 176 | 6. |
| 6000 | 511.6 | 584.5 | 176.4 | 97.7 | 76.1 | 289.4 | 806.3 | 12.3 | • S.C | 85 | Ø | 176 | б, " |
| 6100 | 496.7 | 576.9 | | 95.i | 75.0 | 311.9 | 796.9 | 1i.7 | . 56 | 86 | | 176 | ė. |
| 6200 | 491.6 | 580.3 | 191.7 | 96.0 | 74.4 | 296.4 | 817.0 | 12.7 | .53 | 86 | Ø | 176 | 6. |
| 6300 | 478.6 | 574.i | 199.6 | 95.8 | 73.4 | 311.4 | 828,2 | 12.2 | . 87 | 86 | Ø | 177 | 6 |
| 6400 | 465.1 | 566.8 | 207.6 | 95.6 | 72.3 | 288.5 | 839.0 | 13.4 | . 83 | 85 | Ø | 177 | . 7.: |

Test #11 – Second day, Torque Master plugs, 1" spacer (May 16/97)

- had to abort pull due to severe plug mis firing and blown exhaust gasket -
- plugs seemed to have trouble lighting up mixture at higher RPMs with dramatic loss of power
- noticed that a number of the plug wires were heat damaged from direct contact and/or exposure to high exhaust heat
- after noticing that the #4 header gasket had blown out, 2 more gaskets were damaged during the testing on May 16

LData from computer disk file - (DEREK12)

Standard Corrected Data for 29.92 inches Hg. 60 F dry air Test# 11

| Test: 300 RPM/Sec Acceleration | Fuel Spec. Grav.: | .721 | Air Sensor: 9.0 |
|--------------------------------|----------------------|-------|------------------|
| Vapor Pressure: .33 | Barometric Pres.: | 30.13 | Ratio: 1.00 TO 1 |
| Engine Type: 4-Cycle Spark | Engine displacement: | 502.0 | Stroke: 4.000 |

| REM | CBT | CBHP | FILE | VEZ | ME% | FA+FB | - A1 | AZE | BSFC | CAT | OIL | WAT | BSAC |
|------|--------|-------|-------|-------|---------------|-------|--------|------|------------------|--------|---------------|------|------|
| | Lb-Ft. | | | | | Lb/Hr | នលក៏ព | | | F | Out | Out | |
| 2900 | 515.4 | 284.6 | 46.2 | 86.8 | 85.8 | 143.3 | 355.6 | 11.4 | - 51 | 73 | Ø | 171 | 5.84 |
| 3000 | 508.6 | 287.1 | 48.7 | 84.7 | 85.3 | 152.3 | 358.5 | 10.8 | . 54 | 73 | Ø | 171 | 5.84 |
| 3100 | 497.1 | 293.4 | 51.6 | 85.9 | 84.8 | 150.1 | 375.9 | 11.5 | n shi Ci | | \bigotimes | 171 | 5.99 |
| 3200 | 507.1 | 309.0 | 54.7 | 88.Ø | 84.7 | 155.5 | 397.4 | 11.7 | - SÊ | 73 | 121 | 171 | 6.22 |
| 3300 | 518.8 | 326.0 | 57.7 | 88.2 | 84.7 | 157.2 | 410.9 | 12.Ø | . 49 | 73 | Ø | 171 | 5.90 |
| 3400 | 338.0 | 348.3 | 60.9 | 89.3 | 84.9 | 160.8 | 428.6 | 12.2 | . 47 | 73 | \mathbb{Q} | 171 | 5.76 |
| 3500 | 530.3 | 353.4 | 64.1 | 9Ø.8 | 84.4 | 166.Ø | 448.7 | 12.4 | . 48 | 73 | i2 | 171 | 5.94 |
| 3600 | 536.0 | 367.4 | 67.4 | 92.8 | 84.2 | 167.9 | 471.5 | 12.9 | . 47 | 73 | Ø | 171 | 6.00 |
| 3700 | 543.7 | 383.0 | 70.9 | 93. S | 84.i | 170.2 | 487. Ø | 13.1 | . 455 | 73 | $\sqrt{2}$ | 171 | 5,95 |
| 3800 | 545.0 | 394.3 | 74.3 | 93.3 | 83.9 | 182.6 | 500.S | 18.6 | . 47 | 7,3 | £1 | 1.71 | 5.94 |
| 3900 | 685.7 | 412.6 | 77.7 | 95.5 | 83.9 | 192.2 | 525.8 | 12.6 | . 47 | - 73 | 1Z) | 167 | 5.96 |
| 4000 | 555.7 | 423.2 | 81.3 | 199.1 | 83.6 | 193.7 | 564.8 | 13.4 | . 47 | 73 | Ŵ. | 169 | 6.25 |
| 4100 | 573.8 | 447.9 | 84.9 | 97.9 | 83.8 | 200.0 | 566.2 | 13.0 | . 46 | 73 | Ø | 171 | 5.92 |
| 4200 | 580.0 | 463.8 | 88.5 | 100.6 | 83.7 | 207.5 | 595.3 | 13.2 | a 46 | 74 | Ø | 171 | 6.21 |
| 4300 | 584.5 | 478.6 | 92.3 | 101.6 | 83.5 | 214.i | 615.9 | 13.2 | . 46 | 74 | Ø | 171 | 6.03 |
| 4420 | 578.4 | 484.6 | 96.1 | 101.3 | | | 628.7 | 12.5 | . 4B | 73 | Ø | 171 | 6.03 |
| 4500 | 591.8 | 507.1 | 100.0 | | | 233.0 | 654.0 | 12.9 | . 47 | 73 | Ø | 17E | 6.04 |
| 4600 | 588.8 | 515.7 | 104.0 | 102.9 | 82.9 | 241.3 | 667.8 | 12.7 | . 40 | 73 | \mathcal{D} | 169 | 6.96 |
| 4700 | 588.8 | 526.9 | 108.0 | 102.2 | 82.7 | 242.5 | 676.5 | 12.8 | . 47 | 74 | $\langle O$ | 170 | 6.02 |
| 4860 | 591.4 | 540.5 | 110.1 | 103.9 | | | 203.0 | 18.6 | $: \ell_i \odot$ | 74 | (2) (2) | 172 | 6.10 |
| 4900 | 581.0 | 542.1 | 116.4 | 102.3 | 82 . Ø | 257.4 | 705.8 | 12.6 | "4;*) | 74 | Ø | 172 | 6.11 |
| 5000 | 578.1 | 550.4 | 120.6 | 103.5 | 81.7 | 259.1 | 729.4 | 12.9 | . 48 | 74 | Q1 | 172 | 6.22 |
| 5100 | 574.3 | 557.7 | 125.1 | 101.4 | 81.4 | 251.3 | 729.2 | 13.3 | . 46 | ° / 44 | 12 | 173 | 6.13 |
| 5200 | 562.5 | 556.9 | 129.5 | 102.8 | 80.8 | 260.2 | 752.9 | 13.3 | , 4 <u>9</u> | 74 | ₩2t | 173 | 6.34 |
| 5300 | 553.5 | 558.6 | 134.5 | 101.0 | 80.2 | 250.9 | 754.5 | 13.8 | . 4ts | 74 | Ø | 173 | 6.34 |
| 5400 | 651.4 | 566.9 | 140.1 | 103.3 | 79.8 | 271.5 | 786.4 | 13.3 | . 49 | 73 | Ø | 174 | 6.50 |
| 5300 | 547.3 | 573.1 | 145.9 | 120.4 | 79.4 | 281.0 | 779.2 | 12.7 | . 52 | 73 | Ø | 174 | 6.37 |
| 5600 | 539.9 | 875.7 | 151.7 | | 78.8 | 275.6 | 799.5 | 13.3 | . 49 | 73 | Q | 1.74 | 6.51 |
| 5700 | 528.3 | 573.4 | 187.7 | 101.5 | 78.1 | | 816.0 | 13.8 | . 50 | 73 | 69 | \$74 | 6.68 |
| 5800 | 522.3 | 576.8 | 163.9 | 102.0 | 77.5 | 286.4 | 833.8 | 13.4 | - 51 | 73 | Ų) | 174 | 6.78 |

Test #12 - same as above, aborted as well (May 16/97)

- had to abort pull due to severe plug mis firing again, decided to change back to old plugs and change header gasket again

Data from computer disk file - (DEREK13 >

| Sta | ndard C | ionnecte | ed Data | for | 29.92 | inches | 3 Hg. 64 | ∂ F dry | air | | Test | ; 朴 | t e |
|---------|--------------|---------------|---------|-------|-------|----------------|------------------------------|---------|------|----------|-----------------------|------------|------|
| Vapor 1 | Pressur | | 3 | | Baro | netric | Grav.: Pres.: placemen | 30. | 12 | Rat | Sens io: 1 ske: | | TO 1 |
| RPM | CÉT Lb-Ft | СВНР | FHP | VEX | ME% | FA+FB Lb/Hr | Al scfm | A/F | BSFC | CAT F | OIL Out | WAT Out | DSAC |
| 3800 | 585.8 | 423.8 | 74.3 | | | 194.0 | 520.1 | 12.3 | . 47 | 88 | | 176 | 5.84 |
| 3900 | 571.2 | 4 台4。已 | 77.7 | | 84.2 | | 524.Ø | 12. Ø | .49 | 88 | Ø | | 5.88 |
| 4回回回 | 574.6 | 437.6 | 81.3 | 97.5 | 83.9 | 198.6 | 535.7 | 12.4 | . 47 | 87 | Ø | 175 | 5.82 |
| 4100 | 588.7 | 459.6 | 84.9 | 98.Ø | 84. Ø | 205.5 | 554.6 | 12.4 | . 46 | 85 | Ø | 176 | 5.72 |
| 4200 | 596.5 | 477.10 | 88.5 | 97.8 | 83.9 | 206.2 | 565.3 | 12.6 | .45 | 86 | ίζi | 176 | 5.63 |
| 4300 | 592.3 | 484.9 | 92.3 | 99.3 | 83.5 | 216.7 | 587.6 | 12.5 | . 46 | 66 | Ø | 176 | 5.76 |
| 4466 | 611.0 | 511.9 | 96.1 | 102.2 | 83.7 | 224.4 | 619.2 | 12.7 | . 45 | 86 | 64 | 176 | 5.75 |
| 4500 | 604.4 | 517.9 | 100.0 | 103.3 | 83.3 | 230.3 | 638.4 | 12.7 | , 46 | 87 | Ø | 176 | 5.86 |
| 4660 | 602.2 | 527.4 | 104.0 | 101.9 | 83.0 | 237.0 | 644.4 | 12.5 | . 47 | 37 | Ø | 176 | 5.81 |
| 4700 | 600.5 | 537.4 | 108.0 | 101.3 | 82.8 | 239.1 | 657.2 | 12.6 | . 46 | 87 | Ø | 176 | 5.82 |
| 4888 | 594.3 | 543.2 | 112.1 | 101.1 | 82.4 | 244.8 | 665.4 | 12.5 | . 47 | 87 | Ø | 176 | 5.84 |
| 4900 | 581.5 | 542.5 | 116.4 | 102.4 | 81.8 | 245.1 | 689.6 | 12.9 | . 47 | 87 | Ø | 176 | 6.05 |
| 5000 | 584.8 | 556.7 | 120.6 | | | | 710.2 | 13.3 | . 46 | 87 | 0 | | 6.07 |
| 5100 | 580.1 | 563.3 | 125.1 | | | 245.7 | 784.0 | 13.5 | . 45 | 87 | Ø | 176 | 6.12 |
| 5200 | 565.4 | | | | | 247.6 | | 13.6 | ,46 | 86 | ø | 176 | 6.22 |

Test #13 – back to old plugs (May 16/97)

- this run was a repeat of run #7 from the previous day as a benchmarking run and it resulted in a power loss across the power band of 5-10 ft-lbs of torque and 10 hp at the top end.
- The sheet for this run was lost but this slight loss of power from the previous day was maintained for the remaining tests conducted on day 2 and should be taken into account when comparing results between days.
- The most likely result of this loss of recorded power was a combination of a small change in the dyno setup (repeatability and accuracy), the weather, and possibly (most likely) a change in the engine setup such as the ignition system quality)

<u>Test #14 – removed 1" spacer (May 16/97)</u>

- Noticed no change in power from the (lost) run #13 which indicated that the large volume of the under carb area in the Dart single plane manifold produced optimum power without the addition of further volume

Data from computer disk file - (DEREK15)

| Standard Corrected Data for | | | | a tor á | 29 . 98 | inche | s Hg. (| 60 F dry | air | | Test | ; 朴 | 14 |
|-----------------------------|----------------|---------|---------|---------|----------------|---------|---------|-----------|--------------|------|---------------|------|------|
| Test; | 300 RF | M/Sec f | Accele | ration | Fuel | Spec. | Grav. | 1 .78 | | | Sens | | |
| | Fressur | | | | | netric | | | | Rati | io: 1 | . 00 | TO 1 |
| Engine | Type: | 4-Cycle | a Spark | | Engin | ne disj | olacem | ent: 502. | . Ø | Stri | oke: | 4 6 | 1202 |
| | | | | | | | | | | | | | |
| RPM | CHT | CBHP | FHP | VE% | MEX | FAFB | A1 | AZE | BSFC | | | | BSAC |
| | Lb-Ft | | | | | L5/Hr | scfa | | | F | Out | Out | |
| 3800 | 570.3 | 412.6 | 74.3 | | | 186.9 | | | . 47 | 86 | Ø | 174 | 5.91 |
| 3900 | 561.3 | 416.8 | 77.7 | | | 189.3 | | | .47 | 86 | Q1 | 174 | 5.89 |
| 4000 | 568.2 | 432.7 | 81.3 | | | 197.4 | | 12.6 | . 47 | 86 | (Z) | 174 | 5.96 |
| 4100 | 580.1 | 452.9 | 84.9 | | | 203.5 | | 12.4 | . 47 | 66 | (J | 174 | 5.77 |
| 4200 | 589.1 | 47i.i | 88.5 | | | 209.1 | | | , 46 | 86 | Ø | 175 | 5.75 |
| 4300 | 595.9 | 487.9 | | | | 212.4 | | | 4 | 86 | Ω. | 175 | 5.96 |
| 4400 | 603.3 | 505.4 | 96.1 | | | 226.0 | | | " 46 | 86 | Ø | i73 | 5.92 |
| 4500 | 601.4 | | | | | 234.0 | | | . 47 | 88 | 12 | 175 | 5,94 |
| 4600 | 599.7 | 525.3 | 104.0 | | | 230.9 | | | , 4ta | 86 | Ø | 175 | 5.91 |
| 4700 | 595.5 | 532.9 | 108.0 | 103.0 | 82.6 | 241.2 | 666.0 | 12.7 | . 47 | 36 | 0 | 173 | 5.95 |
| 4800 | 596.8 | 545,4 | 112.1 | 102.4 | 82.4 | 245.6 | 676.7 | | . 47 | 86 | Ø | 175 | 5.90 |
| 4960 | 587.Ø | | | | | 258.4 | | 12.3 | .49 | 86 | 199 | 175 | 6.20 |
| 5000 | 583.8 | | | 100.5 | 81.6 | 245.2 | 692.i | 13.0 | "46 | 36 | Ø | 175 | 5.93 |
| 5100 | 575.6 | 558.9 | | | | 257.9 | | 13.0 | . 4 <u>0</u> | 86 | (Z) | 175 | 6.21 |
| 5200 | 573.9 | 568.2 | 129.5 | 102.5 | 80.9 | 257.5 | 734.1 | 13.1 | . 47 | 86 | \otimes | 175 | 6.15 |
| 5300 | 564.3 | 569.5 | 134.5 | 99.3 | 80.3 | 245. 5 | 725.2 | 13.6 | .45 | 65 | 121 | 175 | 6.V6 |
| 5400 | 562.6 | 578.5 | 140.1 | 101.7 | 79.9 | 276.4 | 757.2 | 12.6 | . 50 | 85 | (2) | 175 | 6.23 |
| 5500 | 33 3. 2 | 581.4 | 145.9 | 102.5 | 79.3 | 283.7 | 776.7 | 12.6 | . 51 | 86 | Ø | 177 | 6.36 |
| 5600 | 548.1 | 584.4 | 151.7 | 103.0 | 78.8 | 271.5 | 793.6 | 13.4 | * 48 | 86 | 0 | 177 | 6.47 |
| 5700 | 537.4 | 583.2 | 157.7 | 102.5 | 78.1 | 885.3 | 805.1 | 13.0 | . 31 | 36 | 12 | 176 | 6.58 |
| 5600 | 528.9 | 584.1 | 163.9 | 98.7 | 77.4 | 292.4 | 788.9 | i 2. 4 | . Se | 86 | \mathbb{Q} | 176 | 6.44 |
| 5900 | - 519.1 | 383.1 | 170.0 | 99.5 | 76.8 | 294.5 | 807.9 | 12.6 | - 49 G | 86 | 创 | 176 | 6.61 |
| 6000 | 508.4 | 580.8 | 176.4 | 97.6 | 76.2 | 294.0 | 806.0 | 12.6 | . 83 | 86 | V2 | 177 | 6.62 |
| 6100 | 496.3 | 576.4 | 184.0 | 96.9 | 75.1 | 238.8 | 814.6 | 13.0 | . SE | 86 | Ø | 176 | 5.75 |
| 6200 | 482.8 | 569.9 | 191.7 | 96.Ø | 74.i | 282.8 | 820.0 | 13.3 | s 22 | 86 | Ø | 176 | 6.87 |
| 6300 | 474.6 | 369.3 | 199.6 | 93.5 | 73.3 | 293.3 | 810.5 | 12.7 | . 54 | 86 | Ø | 176 | 6.80 |
| 6400 | 459.7 | .560.2 | 207.6 | 93.8 | 72.1 | 297.3 | 826.3 | 12.8 | . 55 | 86 | \mathcal{O} | i76 | 7.05 |
| | | | | | | | | | | | | | |

<u>Test #15 – changed to Edelbrock Performer RPM dual plane manifold without a spacer (May 16/97)</u>

- Noticed that the carb was pulling on the venturies much harder with the change to the dual plane manifold and was running rich. This showed that the Dart single plane manifold was less efficient in regards to fuel distribution and quality.

Data from computer disk file - (DEREK16 >

| Sta | ndard (| Jorrecte | ed Data | a for 2 | 29.92 | inche | s Hg. 6 | Ø F dry | air | | Test# | 1.5 | | |
|---------------------|---------|----------|---------|---------|-------|---|---------|---------|----------|---------------------------|--|-------|--|--|
| Vapor Pressure: .33 | | | | | Baror | Fuel Spec. Grav.: .721 Barometric Pres.: 30.10 Engine displacement: 502.0 | | | | | Air Sensor: 5.0 Ratio: 1.00 TO 1 Stroke: 4.000 | | | |
| RPM | CBT | CBHP | PHP | VE% | МЕХ | FA+FB | 11 | A/F | BSFC | | OIL WAT | BSAC | | |
| | Lo-Ft | | | | | Lb/Hr | scfa | | | F. | Out Out | | | |
| 3900 | 594.6 | 441.5 | 77.7 | | | 216.4 | | i1.3 | .51 | 88 | @ 174 | 5.72 | | |
| 4000 | 395.0 | 453. E | 81.3 | 99.Ø | 84.3 | 222.3 | 543.3 | 11.2 | a si i | 88 | 0 174 | 5.71 | | |
| 4100 | 598.1 | 466.9 | 84.9 | | | 218.4 | | 11.6 | . 4B | 87 | @ 174 | 5.61 | | |
| 4200 | 599.5 | 479.4 | 88.5 | | | 225.6 | | 11.7 | .49 | 87 | £ 174 | 5.68 | | |
| 4300 | 596.8 | 488.6 | 92.3 | 99.B | 83.6 | 234.2 | 589.9 | 11.6 | .50 | 87 | @ 174 | 5.74 | | |
| 44810 | 592.5 | . 496. 4 | 96.1 | 98.8 | 83.3 | 234.0 | 597.6 | 11.7 | . 49 | 87 | 囟 175 | 5.73 | | |
| 4500 | 595.9 | 510.6 | 100.0 | 100.7 | 83.1 | 240.9 | 622.8 | 11.9 | . 49 | 87 | 0 175 | 5.80 | | |
| 4600 | 594.7 | 520.9 | 104.0 | 108.1 | 82.9 | 247.1 | 632.8 | 11.8 | "49 | 87 | Ø 175 | 5.78 | | |
| 4700 | 588.5 | 526.6 | 108.0 | 100.5 | 82.5 | 250.9 | 649.3 | 11.9 | .49 | 87 | Ø 175 | 5.87 | | |
| 4800 | 588.Ø | \$37.4 | 112.1 | 101.5 | 62.2 | 255.4 | 669.6 | 18.0 | . 49 | 87 | 0 175 | 5.93 | | |
| 4900 | 574.2 | 535.7 | 116.4 | 101.4 | 81.6 | 259.0 | 682.5 | 12.i | .50 | - 67 | Ø 175 | 6.06 | | |
| 5000 | 575.0 | 547.4 | 120.6 | 99.2 | 81.4 | 265.7 | 681.5 | 11.8 | .50 | 87 | 0 175 | 5.92 | | |
| 5100 | 565.Ø | 548.6 | 125.1 | 100.4 | 80.9 | 273.3 | 704.0 | 11.8 | - SS | 87 | 0 175 | 6.11 | | |
| 5200 | 562.i | 356.5 | 129.5 | 100.4 | 80.6 | 270.5 | 717.6 | 12.2 | . 50 | 87 | 0 175 | 6.14 | | |
| 5300 | 560.9 | 566.0 | 134.5 | 99.8 | 80.2 | 272.3 | 726.6 | 18.3 | .50 | 87 | 0 175 | 6.11 | | |
| 5400 | 531.6 | 567.1 | 140.1 | 99.2 | 79.8 | 273.1 | 735.7 | 12.4 | . 30 | 87 | 0.175 | 6.18 | | |
| 5500 | 546.7 | 572.5 | 145.9 | 100.3 | 79.1 | 284.6 | 757.8 | 12.2 | a thirth | 87 | 0 175 | 6.31 | | |
| 5600 | 531.1 | 566.3 | 151.7 | 100.8 | 78.3 | 283.2 | 779.8 | 12.6 | .32 | $\mathbf{a}_{\mathbf{c}}$ | 0 175 | 6.55 | | |
| 5700 | 524.4 | 569.1 | 157.7 | 101.8 | 77.7 | 289.5 | 799.7 | 12.7 | .53 | 85 | Ø 175 | 6.69 | | |
| 5800 | 517.2 | 571.2 | 163.9 | 97.2 | 77.1 | 289.3 | 776.5 | 12.3 | . 53 | 85 | 0 175 | 6.48 | | |
| 39 0 0 | 504.7 | 567.0 | 170.0 | 98.1 | 76.3 | 290.4 | 797.9 | 12.6 | . 83 | 85 | 0 175 | 6.71 | | |
| 6000 | 498.0 | 568.9 | 178.4 | 94.5 | 75.6 | 292.3 | 781.8 | 12.3 | .53 | 85 | 0 175 | 6.65 | | |
| 6100 | 487.4 | 566.1 | 184.0 | 95.6 | 74.8 | 287.5 | 805.0 | 12.9 | . 83 | 84 | Ø 176 | 6.77 | | |
| 6200 | 471.5 | 556.6 | 191.7 | 95.5 | 73.7 | 292.7 | 817.9 | 12.8 | . 65 | 84 | 0 176 | 7.120 | | |
| 6300 | 452.0 | 542.2 | 199.6 | 93.4 | 72.3 | 300.2 | 812.5 | 12.4 | . 58 | 84 | 0 176 | 7.14 | | |
| 64212 | 442.1 | 538.7 | | | | 306.9 | | 12.2 | . 59 | 84 | Ø 171 | 7.23 | | |

Test #16 - leaned out jets from 76/88 to 74/85 (May 16/97)

- While the power output was still down as much as 10hp from the Dart single plane manifold, there was no change in the rpm power curve shape or peak hp rpm point until past 6000 rpm. The loss in power from the switch in manifolds only started to show up (other than the 5-10 hp across the board which may have been caused by other variables) as a noticeable drop above 6000 rpm which was more than 200 rpm above the hp peak.
- This indicates that the Dart single plane manifold may not hold any appreciable advantage over the operating range of the engine during racing conditions with the current setup (if the 5-10 hp loss was the result of other variables only further testing after the porting of the heads will be able to determine this).
- After porting the heads, a change to a larger cam may favor the Dart single plane manifold at the expense of idle quality and low rpm torque and possibly the same cam may also work better with the single plane manifold.

Data from computer disk file - (DEREK17)

Standard Corrected Data for 29.92 inches Hg. 60 F dry air Test# 16 Test: 300 RPM/Sec Acceleration Fuel Spec. Grav.: .721 Air Sensor: 9.0 Vapor Pressure: .33 Barometric Pres.: 30.10 Ratio: 1.00 TO 1 Engine Type: 4-Cycle Spark Engine displacement: 502.0 Stroke: 4.000 RPM CBT CBHP FHP VEX MEX FA+FB A1 A/F BSFC CAT OIL WAT BSAC Lb-Ft Lb/Hr scfn F Out Out .46 5.09 3800 603.5 436.7 74.3 102.8 85.1 193.8 545.9 12.9 78 Ø 17877.7 102.3 84.5 192.8 557.5 3900 584.0 433.7 13.3 " 4Ev 78 0 178 6.05 4022595.8 453.8 81.3 102.7 84.5 204.8 573.8 12.9 . 46 780 178 5.95 4100 596.6 465.7 84.9 101.8 84.8 205.9 581.9 i3.0 . 45 79 0 178 5.89 . 45 4200 598.0 478. E 88.5 100.5 84.0 211.5 589.7 12.8 78 0 178 5.81 4300 598.5 490.0 92.3 101.1 83.8 221.6 607.4 78 Ø 178 5.84 12.6 . 46 597.7 500.7 96.1 102.7 83.5 224.3 631.7 44120 18.9 **-** 46 78 0 176 5.94 4500 596.3 510.9 100.0 101.1 83.3 229.7 636.0 12.7 . 46 78 0 176 5.86 599.6 525.2 104.0 101.9 83.1 235.4 654.5 46/3/8 12.8 . 46 70 0 178 5.87 45 4788 591.6 529.4 108.0 102.7 82.7 231.7 574.5 13.4 78 Ø 178 6.00 4800 591.2 540.3 112.1 103.7 82.4 245.8 695.8 13.0 . 47 78 177 \mathcal{U} 6.07 543.9 116.4 104.4 82.0 248.2 714.4 4900 583.0 13.2 . 47 78 0 176 6.19 5000 548.4 120.6 102.4 81.6 242.6 715.2 575.0 13.5 . 45 780 175 6.15 SIDA 569.3 552.8 125.1 100.6 81.1 254.5 716.9 12.9 . 47 78 Ø 176 6.11 5200 564.5 558.9 129.5 101.4 80.8 258.8 736.1 13.1 . 48 78 0 176 6.21 5300 554.2 559.3 134.5 101.9 80.2 251.5 754.3 13.8 . 46 78 0 176 5.35 . 48 5400 549.6 565.1 140.1 101.2 79.7 262.2 763.8 13.4 780 176 6.38 5500 546.9 572.7 145.9 100.4 79.3 269.8 771.9 i3.i . 48 78Ø 176 6.36 . 47 540.3 576.1 151.7 100.7 70.7 251.7 786.6 5600 13.8 79 6.45 0 176 5700 531.4 576.7 157.7 96.8 78.0 270.4 769.4 13.1 . 48 79 Ľ٨ 176 6.30 94.9 77.4 278.3 767.1 5800 522.3 576.8 163.9 12.7 79 . 30 0 177 6,29 79 5900 513.3 576.6 170.0 97.9 76.7 281.1 805.6 13.2 . 50 0 177 6.60 . 48 Ø 177 6000 501.6 573.0 176.4 96.9 75.9 267.7 810.5 13.9 79 5.69 . 51 6100 483.4 561.5 184.0 95.2 74.7 277.3 808.1 6.82 13.4 30 0 176 . 50 6200 475.4 561.2 191.7 94.3 74.0 271.2 814.6 13.8 79 Ø 176 6.87 553.8 199.6 95.5 72.9 274.9 839.2 6300 461.7 14.0 . 51 79 Ø 176 7.17 6400 447.4 545.2 207.6 94.1 71.6 273.7 839.4 79 Ø 175 14.1 . 32 7.29

<u>Test #17 – low RPM pull (May 16/97)</u>

- Look at that torque!
- As was typical of the last 2-3 pulls, ignition quality started to degrade with some backfiring and misfiring. This no doubt caused some of the power loss that was indicated during these last tests. A complete tear down of the heads and ignition system before the next dyno session should indicate the cause of this effect.

| Data from computer disk file - (DEREK18) | | | | | | | | | | | | | | |
|---|--------------|---------|---------|----------------------------|-------------------------|---------------------|------------|-------|-----------------|------------------|--------------------|------|--|--|
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| Standard Corrected Data for a | | | | | | 29.92 inches Hg. 60 | | | air | Test# | | 17 | | |
| Test: | | M/Sec F | leceler | ~ation | | | | 21 | Air Sensor: 9.0 | | | | | |
| | | | | | Barometric Pres.: 30.10 | | | | | Ratio: 1.00 TO 1 | | | | |
| Engine Type: 4-Cycle Spark | | | | Engine displacement: 502.0 | | | | | | Stroke: 4.000 | | | | |
| RPM | CBT Lb-Ft | СВНР | FHP | VEX | MEX | FA+FB Lb/Hr | Ai scfm | ∩/F | BSFC | CAT F | OIL WAT Out Out | BSAC | | |
| 3200 | 572.5 | 348.8 | 54.7 | 9.0 B | na 1 | 149.8 | | 13.4 | | r 82 | Ø 174 | 5.90 | | |
| 3300 | 569.8 | 358.0 | 57.7 | | | 161.4 | | 12.9 | . 46 | 80 | 0 174 | 5.98 | | |
| 3400 | 575.9 | 372.8 | 60.9 | | | 166.9 | | 12.6 | . 46 | 80 | 0 174 | 5.78 | | |
| 3500 | 577.5 | 384.9 | 64.1 | | | 167.3 | | 12.7 | 43 | 80 | 0 174 | 5.69 | | |
| 3600 | 581.0 | 398.2 | 67.4 | | | 172.1 | | 12.8 | . 44 | 80 | @ 173 | 3.70 | | |
| 3700 | 583.5 | 411.1 | 70.9 | 97.8 | 84.9 | 176.6 | 503.5 | 13.1 | , ly dy | 80 | Ø 173 | 5.78 | | |
| 3800 | 584.1 | 422.6 | 74.3 | 98.9 | 84.7 | 184.1 | 522.8 | 13.0 | . 45 | 80 | 0 173 | 3.84 | | |
| 3900 | 584.5 | 434.0 | 77.7 | 101.3 | 84.4 | 189.7 | 549.7 | 13.3 | . 45 | 80 | 0 173 | 5.98 | | |
| 4000 | 580.5 | 442.1 | 61.3 | 100.6 | 84.1 | 198.3 | 560.2 | 13.0 | " 4S | 80 | 0 173 | 3.98 | | |
| 4100 | 582.5 | 454.7 | 84.9 | 98.5 | 83.9 | 198.1 | 562.0 | 13.0 | . 43 | 80 | \$ 174 | 5.83 | | |
| 4200 | 587.3 | 469.7 | 88.5 | 98.2 | 83.8 | 206.4 | 574.3 | 12.8 | . 45 | 88 | 0 174 | 5.77 | | |
| 4300 | 589.6 | 482.7 | 92.3 | 99.7 | 83.6 | 213.6 | 596.7 | 12.8 | . 46 | 80 | 0 174 | 5.84 | | |
| 44602 | 587.4 | 498.1 | 96.1 | 101.4 | 83.3 | 219.9 | 620,7 | 13.0 | 。46 | 80 | 0 174 | 5.96 | | |
| 4500 | 587.2 | 503.1 | 100.0 | 102.6 | 83.0 | 224.9 | 642.7 | 13. i | . 46 | 80 | Ø 174 | 6.03 | | |
| 4600 | 586.5 | 513.7 | 104.0 | 103.9 | 82.8 | 231.3 | 664.9 | 13.2 | " 本(E) | 80 | Ø 174 | 6.11 | | |
| 4700 | 586.8 | 525.1 | 108.0 | 101.6 | 82.5 | 234.6 | 664.2 | 13.0 | " 46 | 80 | 0 174 | 5.97 | | |
| 4820 | 585.3 | 534.9 | 112.1 | 102.8 | 82.3 | 241.3 | 686.7 | 13.1 | . 46 | 30 | 0 174 | 6.06 | | |
| 4900 | 581.1 | 542.2 | 116.4 | | | 242,9 | | 13.1 | . 46 | 80 | Ø 174 | 6.06 | | |
| 561212 | 572.9 | 545.4 | | | | 251.Ø | | 12.5 | " 47Z | 日間 | Ø 175 | 5.94 | | |
| 5100 | 563.5 | | | | | 254.3 | | 12,9 | . 48 | 80 | 0 175 | 6.18 | | |
| 5200 | 548.5 | 543.1 | 129.5 | | | 257.0 | | 12.9 | .49 | 9.6 | 0 175 | 6.29 | | |
| 5300 | 534.6 | \$39.5 | | 98.4 | 79.6 | 260.0 | 726.0 | 12.8 | - . 50 | 80 | Ø 175 | 6.36 | | |
| 5400 | 547.9 | 563.3 | | | | 266.3 | | 12.5 | . 49 | ରହ | 0 175 | 6.iØ | | |
| 5500 | 035.0 | 560.8 | | 97.8 | | 263.6 | | 13.0 | . iq (3 | 80 | Ø 175 | 6.31 | | |
| 5600 | 517.6 | 551.9 | | 99.6 | | 275.6 | | 12.9 | .51 | 812 | 0 176 | 6.63 | | |
| 5700 | 507.1 | S9.4 | 157.7 | 97.8 | 77.2 | 272.4 | 775.9 | 13.1 | - 51 | 96 | Ø 176 | 6.67 | | |
| 5800 | 516.7 | 570.6 | | | | 267.4 | | 13.6 | . 43 | 80 | @ 176 | 6.39 | | |
| 5900 | 486.2 | 546.2 | | | | 283.0 | | 12.8 | . 53 | 8Ø | Ø 176 | 6.86 | | |
| 6000 | 478.8 | 547.0 | | | | 590° Ø | | 13.2 | . 53 | 80 | 10 176 | 6.96 | | |
| 6100 | 456.8 | 530.6 | | | | 278.3 | | 13.3 | . 54 | 79 | Ø 177 | 7.17 | | |
| 6220 | 447.9 | 528.7 | | | | 280.2 | | 13.1 | .83 | 79 | Ø 177 | 7.16 | | |
| 6300 | 363.6 | 436.2 | | | | 275.3 | | 13.3 | .65 | 79 | Ø 178 | 8.58 | | |
| 6400 | 362.9 | 442.2 | 207.6 | 89.4 | 67.3 | 274.9 | 798.0 | 13.3 | . 64 | 79 | 0 178 | 8.57 | | |

Test #18 - 2" spacer (May 16/97)

The addition of the spacer resulted in a moderate increase in the mid-range torque but no top end power change

Data from computer disk file - (DEREK19 >

| | Sta | ndard (| Correctu | ed Oab | a for i | 99.92 | inche | s Hn. : | 60 F dry | air | | Test | : 俳 | 18 |
|---|--------|-----------------|----------|---------|---------|-------|---------|---------|----------|--------------------|-------------------|-------------------------|-----|------|
| | | | | | | | | | | | | | | |
| | | | M/Sec (| | | | | | | | | Sens | | |
| | | | °e: " | | | | netric. | | | | | | | TO 1 |
| | cograe | iype: | 4-Cycle | e Spari | < | Engin | ne disp | Diacem | ent: 502 | a 1/3 | 510 114 | oke: | 4.0 | NOVO |
| | RPM | CDT | СВНР | FHP | 9E% | MEX | FAHEB | A1 | A/F | BSFC | CAT | OIL | WAT | BSAC |
| | | Lb-Ft | | | | | Lb/Hr | ទ៤៩៣ | | | i den | Out | Out | |
| | 3900. | -5 / &.5 | 428.1 | 77.1 | 100.3 | 84.2 | 187.2 | 539.4 | 13.2 | . A S | 85 | - 23 | 172 | 5.98 |
| | 4000 | 503.0 | 444.10 | 81.3 | 96.8 | 84.1 | 189.5 | 534.0 | 12.9 | . Lj. Lj. | 85 | 63 | 172 | 5.71 |
| | 4100 | 392.5 | 462.5 | 84.9 | 97.6 | 84.1 | 199.5 | 552.7 | 12.7 | a de 🙄 | 84 | (2) | 172 | 5.67 |
| 6 | 4200 | 602.1 | 481.5 | 88.5 | 103.0 | 84.0 | 200.3 | 598.2 | 13.7 | . 43 | 34 | Ø | 172 | 5.89 |
| | 4300 | 598.2 | 489.8 | 92.3 | 103.2 | 83.7 | 202.6 | 513.0 | i3.9 | . 43 | $\in \mathcal{B}$ | 辺 | 172 | 5.94 |
| | 4400 | 601.4 | 503.8 | 96.1 | 103.4 | 83.5 | 211,3 | 627.3 | 13.6 | . 43 | 84 | Ø | 172 | 5.91 |
| | 4500 | 609.8 | 522.5 | 100.0 | 105.2 | 83.3 | 219.5 | 652.9 | 13.7 | . 43 | 84 | 121 | 172 | 5.93 |
| | 4600 | 598, Ø | 523.8 | 104.0 | 107.1 | 83.0 | 214.2 | 679.6 | 14.6 | . 48 | 84 | Ø | 172 | 6.16 |
| | 47210 | 599.3 | 536.3 | 108.0 | 103.3 | 82.8 | 221.7 | 669.7 | 13.9 | .43 | 84 | Q) | 173 | 5.93 |
| | 4808 | 592.2 | 541.2 | 112.1 | 108.2 | 82.4 | 227.7 | 677.3 | 13.7 | <u>,</u> 44 | 84 | Ø | 173 | 5.94 |
| | 4980 | 588.1 | 540.7 | 116.4 | 104.7 | 82.0 | 242.7 | 707.9 | 13.4 | . 46 | 84 | 121 | 173 | 6.12 |
| | 5000 | 589.5 | 561.2 | i20.6 | 105.1 | 81.8 | 237.4 | 727.0 | 14.1 | · Li Zi | 83 | Ø | 173 | 6.14 |
| | 5100 | 579.0 | 562.2 | 125.1 | 105.9 | 81.3 | 246.9 | 746.5 | 13.9 | . 45 | 83 | 凶 | 174 | 6.30 |
| | Seez | 573.1 | 567.4 | 129.5 | 103.5 | 88.9 | 837.9 | 743.7 | 13.2 | . 47 | 83 | 63 | 174 | 6.22 |
| | 5300 | 557.9 | 563.0 | 134.5 | 102.6 | 80.2 | 258.2 | 732.4 | 13.4 | . 47 | 83 | $\overline{\mathbb{C}}$ | 174 | 6.34 |
| | 5400 | 358.5 | 574. ĉ | 140.1 | 102.4 | 79.9 | 278.7 | 764.7 | 18.6 | .50 | 83 | \$ | 174 | 6.38 |
| | 5500 | 548,8 | 574.7 | 145.9 | 180.1 | 79.2 | 275.7 | 761.6 | 12.7 | .50 | 83 | (Z) | 174 | 6.29 |
| | 5600 | 540.2 | 576.0 | 151.7 | 99.6 | 78.6 | 276.2 | 771.4 | i2.8 | . 50 | 83 | Ø | 174 | 6.36 |
| | 5700 | 528.6 | 573.7 | 157.7 | 99.3 | 77.9 | 272.0 | 782.7 | 13.2 | . 49 | 83 | Ø | 174 | 6.48 |
| | 5800 | 520.4 | 574.7 | 163.9 | 97.3 | 77.2 | 273.9 | 780.0 | 13.1 | , 49 | 83 | Ø | 174 | 6.45 |
| | 5900 | 511.2 | 574.3 | 170.0 | 99. S | 76.5 | 279.1 | 809.4 | 13.3 | . 50 | 83 | 121 | 175 | 8.70 |
| | 6000 | 501.5 | 572.9 | 176.4 | 97.5 | 75.8 | 274.2 | 828.8 | 13.5 | . 50 | 83 | 2 | 175 | 6.71 |
| | 6100 | 482.6 | 560.5 | 184.0 | 93.6 | 74.6 | 267.6 | 789.5 | :3.5 | . 4 ⁵) | 83 | Z | 175 | 6.70 |
| | 6200 | 464.9 | 548.8 | 191.7 | 94.2 | 73.4 | 277.2 | 807.7 | 13.4 | .52 | 83 | \mathcal{Q}_1 | 176 | 7.00 |
| | 6320 | 459.7 | 551.4 | 199.6 | 93.4 | 72.7 | 267.9 | 813.7 | 13.9 | * 30 | 83 | (2) | 176 | 7.03 |
| | 6400 | 420,0 | 511.8 | 207.6 | 93.5 | 70.3 | 274.7 | 827.Ø | 13.8 | . 56 | 83 | Ø | 176 | 7.71 |